

Farabaugh Engineering and Testing Inc.

Project No. T166-97-A

Dade County Notification No. FET97005

Laboratory Certification No. 96-0213.03

Report Date: November 26, 1997

Report Revision Date: July 11, 2018

PROTOCOL PA-125-95 PER

ASTM 1592-95

STANDARD TEST METHOD FOR

STRUCTURAL PERFORMANCE OF SHEET METAL ROOF AND SIDING SYSTEMS BY UNIFORM STATIC AIR PRESSURE DIFFERENCE

On

Peterson Aluminum Corp. Tite-Loc Plus Standing Seam Roof Panel

22 GA/ 16" WIDE

FOR

Petersen Aluminum Corp.

10551 PAC Rd.

Tyler, TX 75707

Report Prepared By:

Patrick J. Farabaugh

Approved By

Daniel G. Farabaugh









ASTM 1592-95

STANDARD TEST METHOD FOR

STRUCTURAL PERFORMANCE OF SHEET METAL ROOF AND SIDING SYSTEMS BY UNIFORM STATIC AIR PRESSURE DIFFERENCE

<u>Purpose</u>

This test method covers the evaluation of the structural performance of Sheet Metal. Panels and Anchor to Panel Attachments for roof or siding systems under uniform static air pressure difference.

Test Dates

Specimen "A" 11-10-97

Specimen "B" 11-11-97

Specimen "C" 11-12-97

Specimen "D" 11-13-97

Test Specimen

Manufacturer: Petersen Aluminum Corp.

10551 PAC Rd.

Tyler, TX 75707

Panel: 22 GA Petersen Aluminum Corp. Tite-Loc Plus Standing Seam Roof Panel 16" Wide

Clip: Low Floating Clip

Span Conditions: 3 Spans@ 5'-0" oc., Both Ends Open (Specimens A, B, C)

12 Spans @ 1'-0" oc. One End Fixed, One End Open (Specimen D)

Testing Apparatus

Test Chamber: Vacuum Chamber Composed of Wood

Mounting Frame: 16 ga Hat Shape Subgirts fastened to W6 X 15 Wide Flange Beams.

Pressure Indicator: Digital Pressure Indicator from Micro-Pneumatic Logic, Inc. with accuracy to one tenth of an inch and traceable to the National Bureau of Standards.

Deflection Dials: Dial Indicators from Starrett, Fowler, CDI and Teclock with accuracy to 0.001 of an inch, certified by Do-All Gage Block #6125 traceable to the National Bureau of Standards.

Installation

- The panels were installed with clips onto 16 ga Hat shape Subgirts using (2) 1/4 -.14 x 1-1/4" SDS fasteners per clip: The side joints consisted of the female rib interlocking with the male rib and seamed with a mechanical seamer. Continuity fasteners were located at the side joints at panel ends.
- The system was inverted and attached to the steel beams with #14 tek fasteners and C- Clamps.
- Plastic (4 mil thick) was employed was employed loosely between the panels and subgirts and in the side joints to create a vacuum seal.

Procedure

- The specimen was checked for proper adjustment and all vents closed in the pressure measuring lines.
- The required deflection measuring devices were installed at their specified locations.
- A nominal initial pressure was applied equal to at least four times but not more than ten times the dead weight of the specimen. This nominal pressure was used as the reference zero and initial deflection readings were recorded.
- At each load increment, pressure was maintained for a period of not less than 60 seconds and until the deflection gages indicated no further increase in deflections.
- Successive increments were achieved as above until failure of the specific ultimate load was reached.

The test was conducted according to the procedure in ASTM E-1592-94 and as noted herein. In our opinion the tape and plastic had no influence on the results of the test.

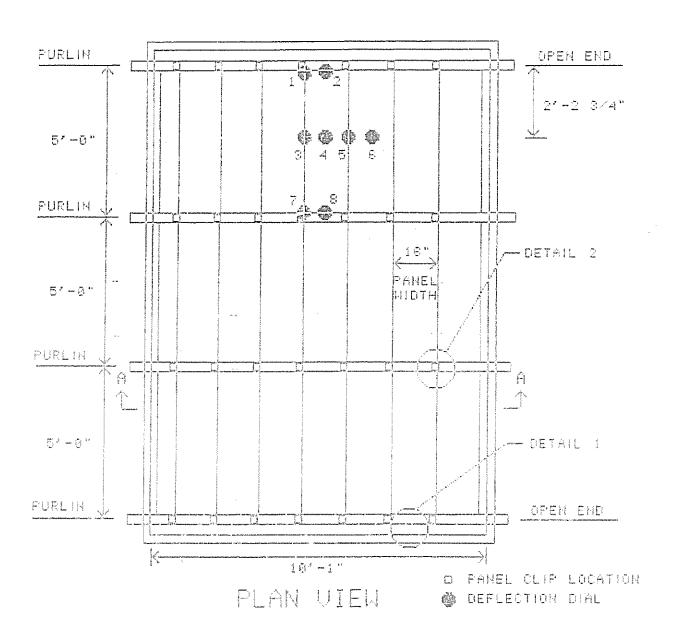
Test Witness: Daniel G. Farabaugh, PE Florida PE #0048349

401 Rosecrest Drive

Monroeville, PA 15146

Reference

This test report references the original test report T166-97, dated 11-26-97 for MBCI for all data and specimen information provided here-in. The customer named in this report, Petersen Aluminum Corp. is authorized by MBCI for use of this test data.

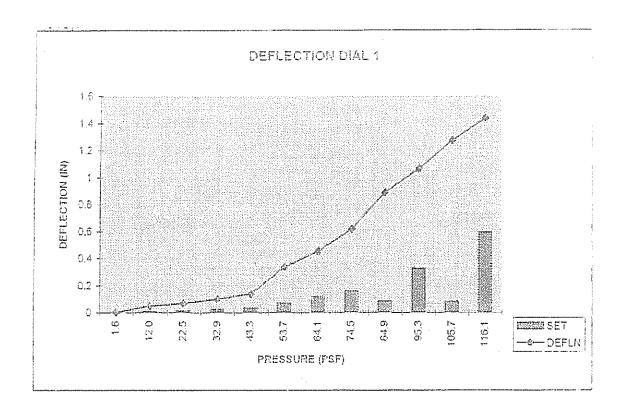


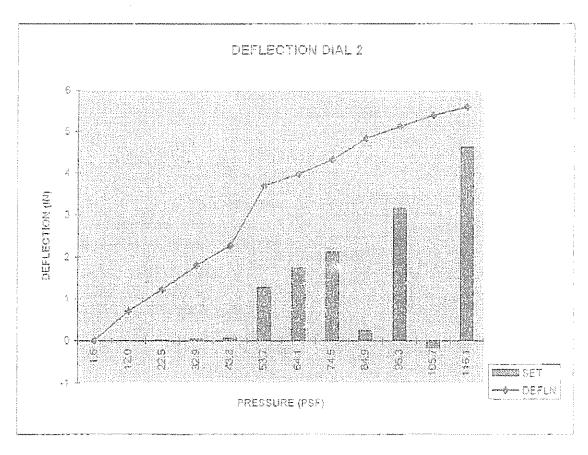
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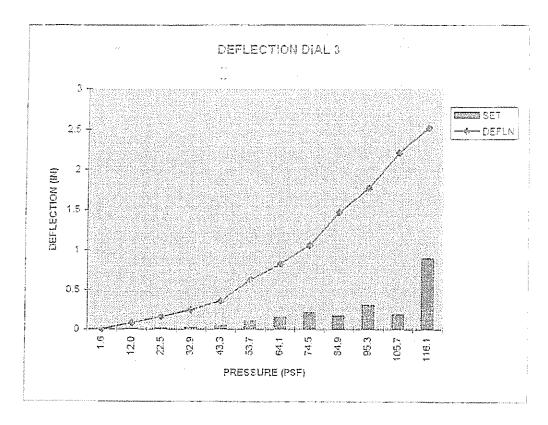
	TEST D	ATA FOR	: 16" PAI	VEL 22 G	A 3SP.	ANS @ 5	-0" pc (S	PEC. A)	
	DEFLEC	TON DI	AL READ	INGS ((INCHES)				
LOAD (PSF)	DIAL 1	DIAL 2	DIAL 3	DIAL 4	DIAL 5	DIAL 6	DIAL 7	DIAL 8	REMARKS
Person (in the second person of the second person o									
1.6	0	O.	0	0	0	0	Û	0	PANEL WT.
12.0	0,049	0.704	0.079	0.48		0.432	0.02	0.316	
1.6	800.0	-0.013	0.009	0.011	0.019	0.024	0.004	0.012	PANEL WT.
22.5	0,068	1.219	0.161	1,111	0.226	1.049	0.062	0.944	
1.6	0.014	0.003	0.012	0.025	0.022	0.047	0.016	0.044	PANEL WT.
32.9	0.1	1.791	0.248	1,736	0.31	1,635	0.11	1,555	
1.6	0.024	0.035	0.022	0.059	0.031	0.092	0.023	0.093	PANEL WT.
43.3	0.137	2.27	0.36	2,232	0.414	2,159	0.167	2.11	
1,5	0.032	0.064	0.041	0,096	0.058	0,141	0.034	0.115	PANEL WT.
53.7	0.338	3.691	0.631	3.786	0.713	3.849	0.472	3.672	
1,6	0.069	1.266	0.108	0.844	0.081	-0.166	0.055	0.446	PANEL WT
54.1	0.453	3,973	0.826	4.111	0.882	3.946	0.61	3.983	
1.6	0.116	1.737	0.152	1.22	0.108	-0.269	0.1	0.745	PANEL WT.
74.5	0.519	4.322	1.06	4.494	1,098,	4.341	0.825	4.367	
1.6	0.157	2.112	0,214	1.563	0.138	-0.321	0.128	1.004	PANEL WT.
84.9	0.889	4.827	1.47	5.053	1.486	4.895	1.201	4,933	
1.6	0.086	0.241	0.172	0.184	0.23	1.649	0.135	0.163	PANEL WT.
95.3	1.065	5,118	1.771	5.417	1.814	5.344	1.552	4 * v · * * - 4 - 4 mi v v 2 * 2 4 · *	
1.6	0.327	3.163		1.97	0,248	4.431	0.181	. 2 . 2	PANEL WT.
105.7	1,273	5.386	*********	5.823	2.21	5,724	****************	5.835	
1.6	0.08	-0.182	0.191	-0.225	0.425	2.488	0,199		PANEL WT.
116.1	1,434	5.596	2.516	6.012	2.552	5.005	2,398		
7.6	0.593	4.623	0.895	4,414	0.954	4.479	0.949	4.385	PANEL WT.
141.6									CLIP
									FAILURE

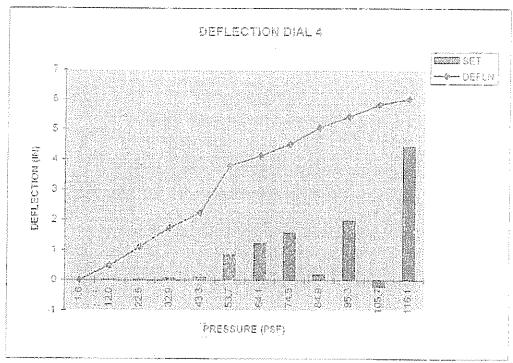
NOTE: PRIOR TO CLIP FAILURE, A LOAD OF 136,9 PSF WAS HELD FOR 1 MIN.

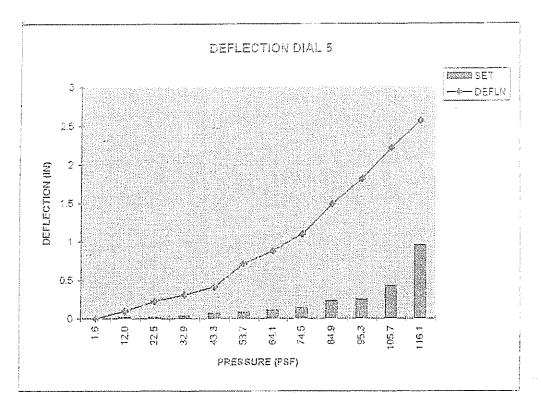
NOTE: SEE SKETCH 1 FOR LOCATION OF CLIP FAILURE.

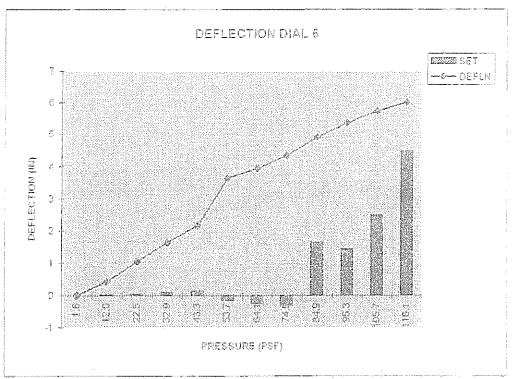


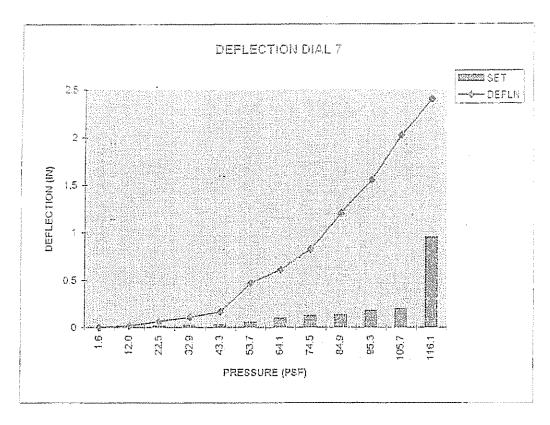


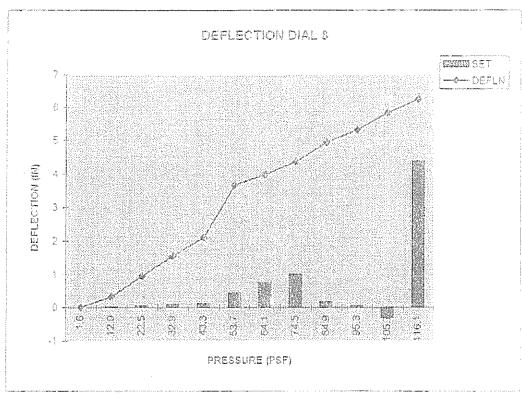


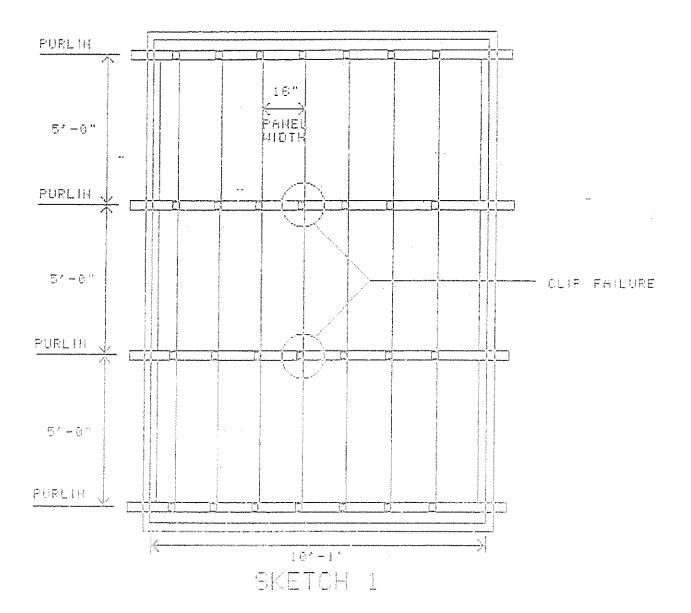








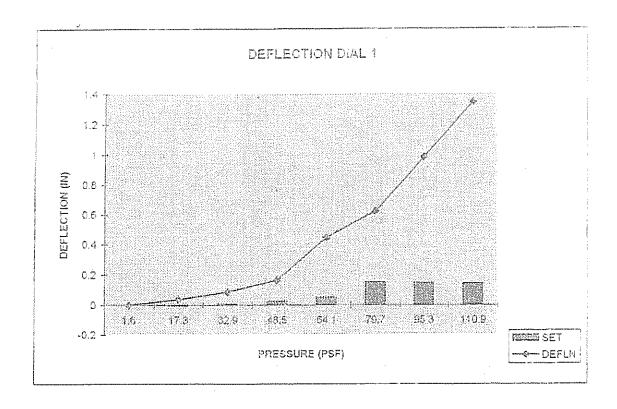


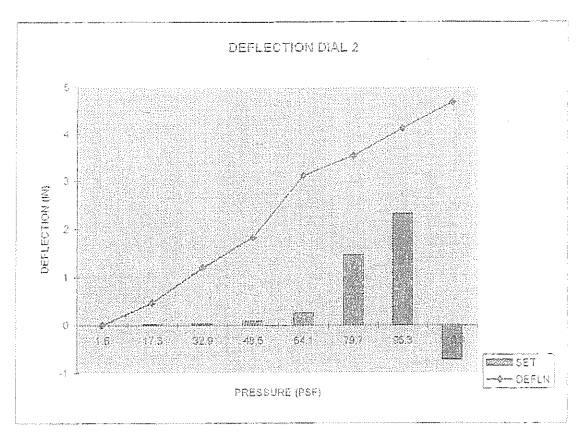


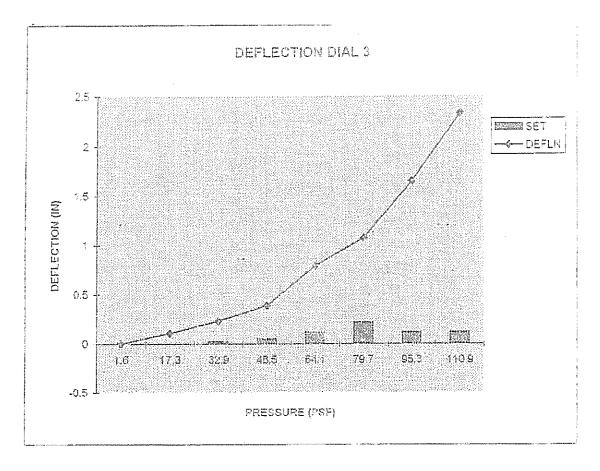
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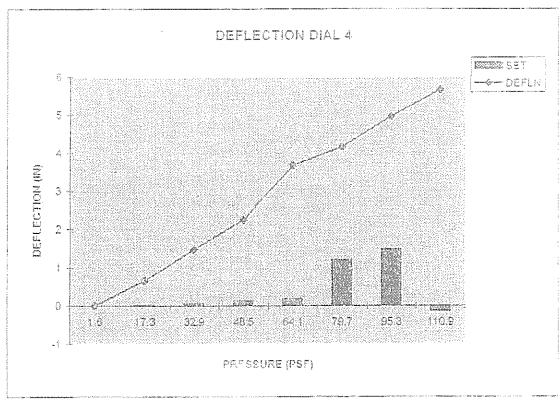
	TEST D	ATA FOR	16" PAI	VEL 22 G	A 3 SPA	NS @ 5	'-0" oc (S	PEC. 5)	
\$40.20:44-4:44-4874-4-800	DEFLEC	NOTICE	AL READ	INGS ((INCHES)				
LOAD (PSF)	DIAL 1	DIAL 2	DIAL 3	DIAL 4	DIAL 5	DIAL 6	DIAL 7	DIAL 8	REMARKS
	een, on the second seco								, , , , ,
1.6	0	0	0	0	0	0	0	0	PANEL WT.
17.3	0.037	0.476	0.105	0.662	0.12	0.701	0.02	0.584	
1.6	-0.006	0.022	-0.001	0,008	0.014	0.016	-0.001	0.021	PANEL WT.
32.9	0.086	1,193	0.23	1.472	0.242	1,47	0.07	1.412	} >> >>
1.6	0.007	0.033	0.023	0.056	0.023	0.047	0.011		PANEL WT.
48.5	0.163	1.825	0,385	2.247	0.404				**>><=!
1.6	0.025	0.085	0.045	0.122	0.042			14.4.244	PANEL WT.
64.1	0.444	3,12	0.789	3.678	0.771	3.727			
1.6	0,05	0.256	0.113	0.185				0.11	PANEL WT.
79.7	0,619	3.542	1.069	4.161	Contraction of the contraction of			\$1	1 a contract of the contract o
1.6	0.151				7411-711-711-1-1-1-1-1-1-1	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	200000000000000000000000000000000000000		PANEL WT.
95.3	0.982	4,124	1,648	4.903	1.715				
1.6	0.145	2.313	0.114	1.489	-0,035	-0,248	-0,035	-0,198	PANEL WT.
110.9	1,345	4.679	2,328	5.657		and the second second second		6.066	5
1,6	0,143	-0.727	0.115	-0,143	0.236	1,852	0.151	-0.262	PANEL WT.
123.4									CLIP
								To the Control of the	FAILURE

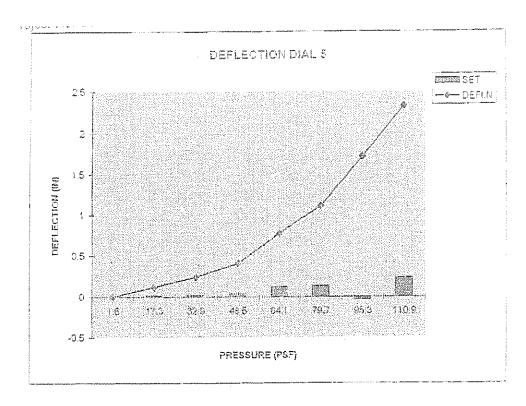
NOTE: SEE SKETCH 2 FOR LOCATION OF CLIP FAILURE.

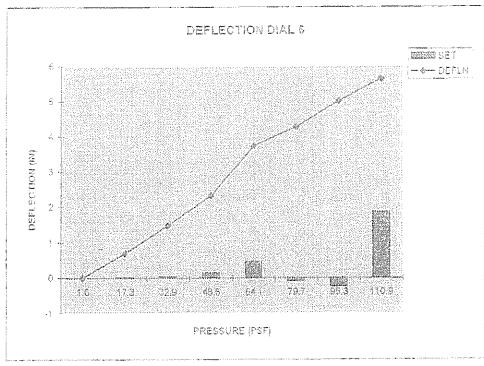


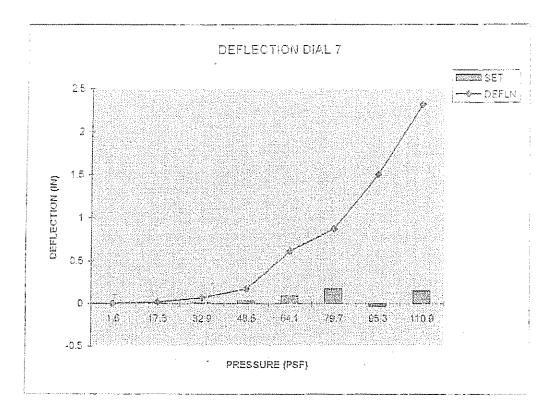


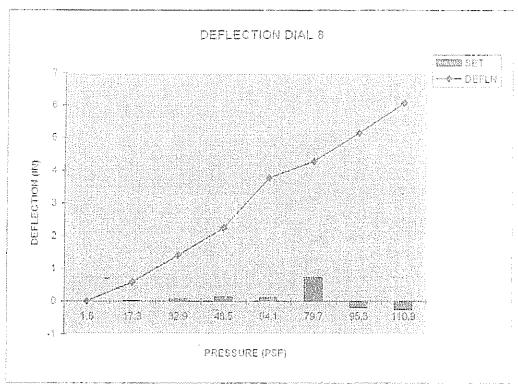


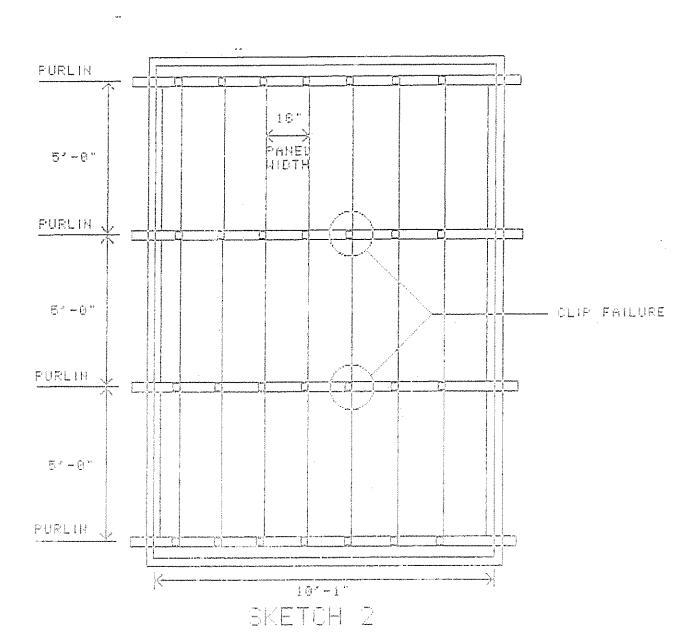






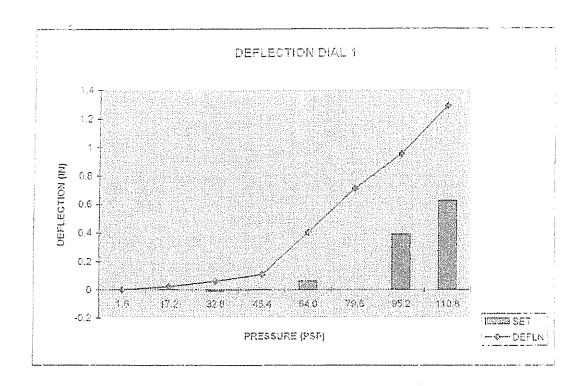


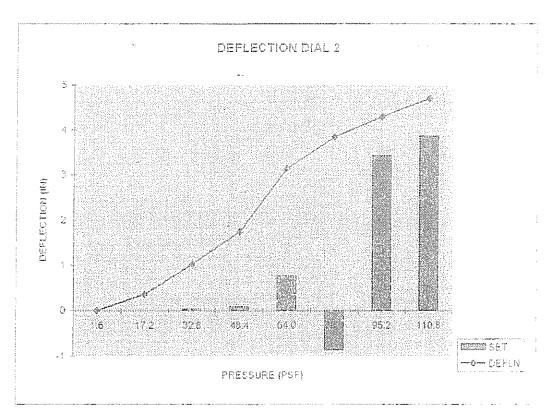


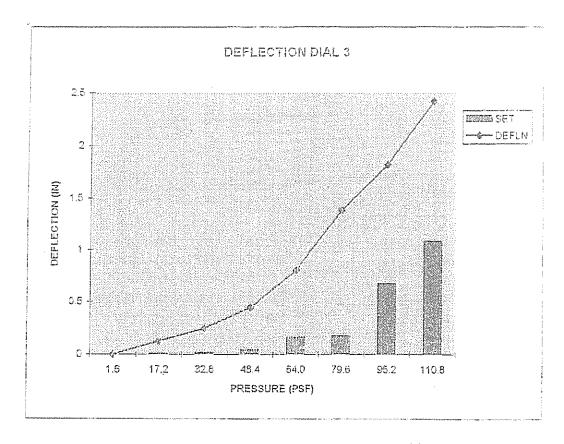


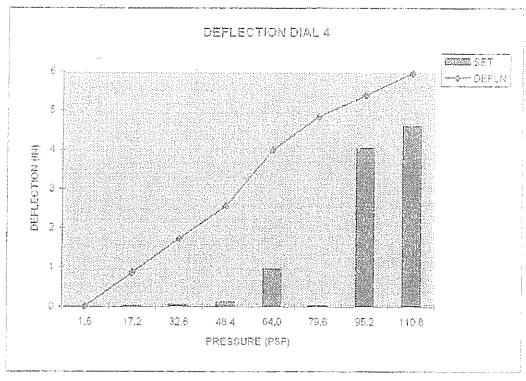
	TEST DA	ATA FOR	16" PA	NEL 22 G	A 3 SP	ANS @ 5	'-0" oc (S	SPEC. C)	
DEFLECTION DIAL READINGS (INCHES)									
LOAD (PSF)	DIAL 1	DIAL 2	DIAL 3	DIAL 4	DIAL 5	DIAL 6	DIAL 7	DIAL 8	REMARKS
\$ \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			jar tjaran (n. 6 a. 6		# (455)361#5554461 - 41 # T			:	
1.6	Ō	0	0	Ō	0	0	0	0	PANEL WT.
17.2	0.022	0.354	0.123	0.857	0.113	0.74	0.075	0.747	
6,1	-0.002	-0.003	0,009	0.009	0.007	0.013	0.003	0.015	PANEL WT.
32.8	0.061	1.023	0.247	1.724	0.261	1.643	0.154	1.657	
1,6	-0.012	0.025	0,019	0.045	0.019	0.054	0.01	0.028	PANEL WT.
48.4	0.107	1.738	0.443	2.562	0.428	2.711	0.264	2.637	
1.6	0.002	0.082	0,042	0.114	0.046	0.144	0,03	0.069	PANEL WT.
64.0	0.402	3.134	0.804	3.988	0.815	4.02	0.72	4.023	
1.6	0,063	0.762	0:161	0.945	0.082	0.119	0.111	0.513	PANEL WT.
79.6	0.709	3.84	1.384	4.84	1.441	4,923	1.301		
1.6	100.0	-0.869	0.178	0,023	0.204	1.155	0.175	-0.219	PANEL WT.
95.2	0.952	4.295	1.818	5.389	2.044	5.545	1.843	5,602	Av
1.6	0,389	3.43	0.676	4,046	0.645	3,84			PANEL WT.
110.8	1.285	4,692	2.417	5,96	2.444	6.086	2.566	6.395	
1.6	0.624	3.863	1,088	4.602	1.158	4,956	1.217	4.791	PANEL WT.
121.2								CLIP	FAILURE
:		163					AND	SCREW	PULLOUT

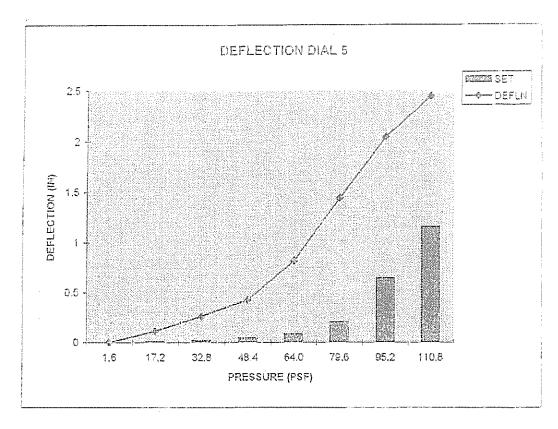
NOTE: SEE SKETCH 3 FOR LOCATION OF CLIP FAILURE AND SCREW PULLOUT.

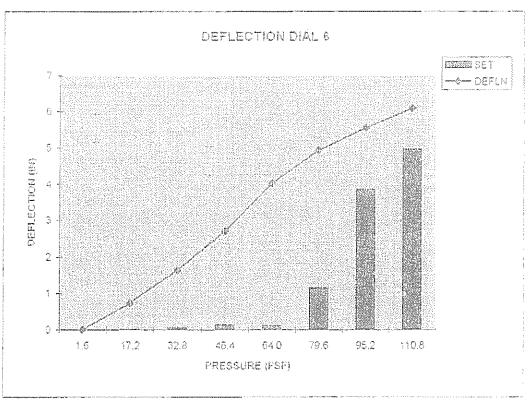


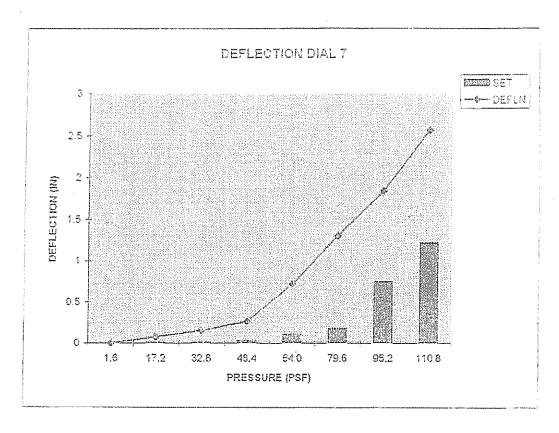


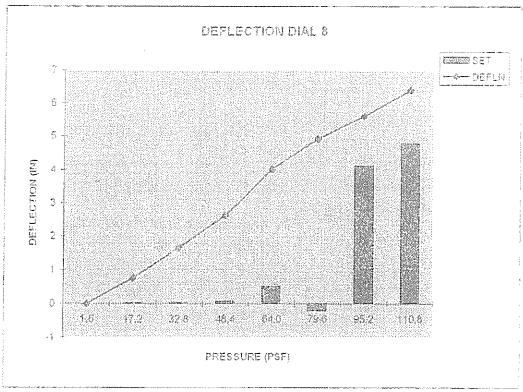


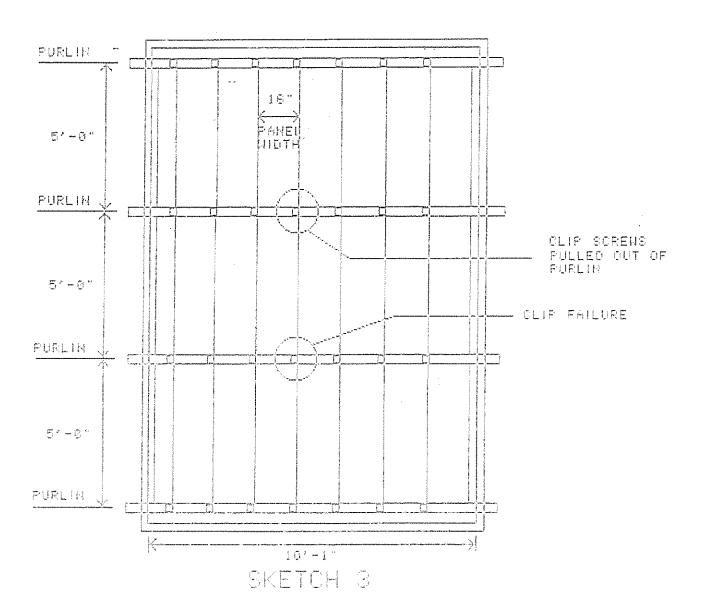




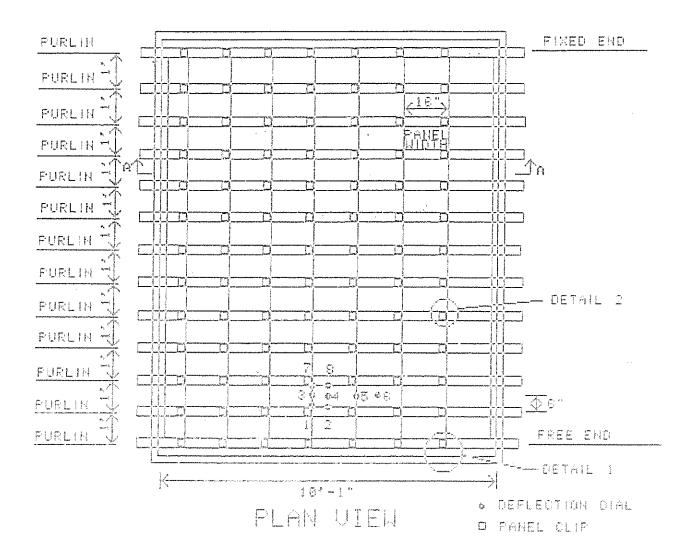








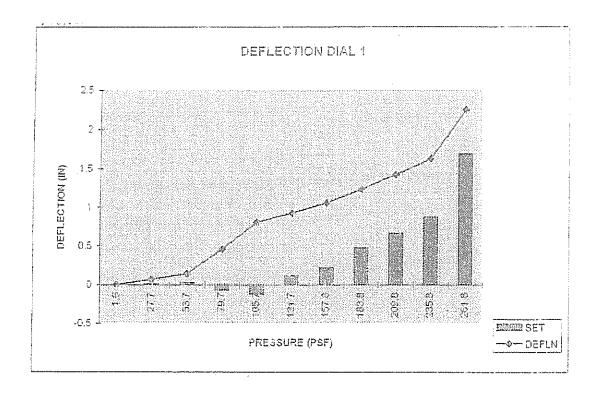
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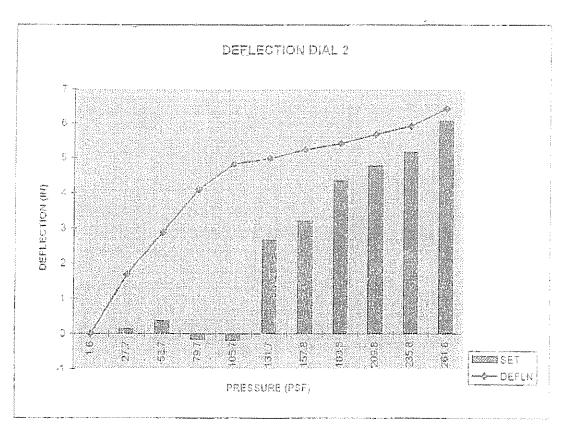


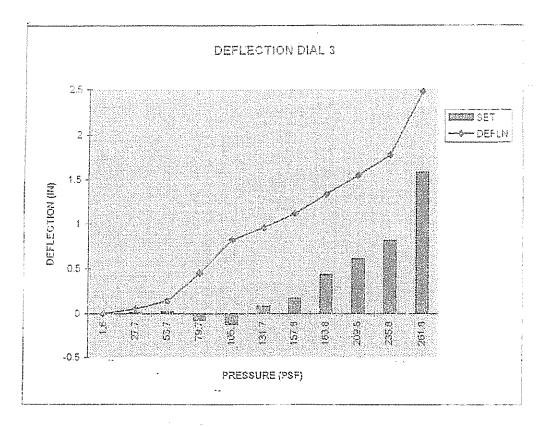
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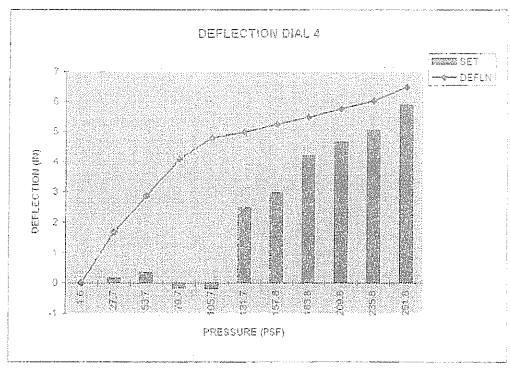
**************************************	TEST D	ATA FOR	16" PAI	VEL 22 G	A 12 SP	ANS @	'-0" oc (SPEC. D	t an income for automorphic property of the common property in the common temporal to the common temporal to the common temporal temporal to the common temporal temp
	DEFLEC	TION DIA	AL READ	INGS	(INCHES)				
LOAD (PSF)	DIAL 1	DIAL 2	DIAL 3	DIAL 4	DIAL 5	DIAL 6	DIAL 7	DIAL 8	REMARKS
				<u>:</u>					
1.6	0	0	Ũ	0	0	0	0	0	PANEL WT.
27.7	0.059	1.686	0.05	1.689	0.02	1.062	0.095	1.683	
1.5	0.014	0.139	0.013	ი.15	-0.004	0.009	0.013	0,155	PANEL WT.
53,7	0.146	2.881	0,144	2.849	0.104	2.221	0.151	2.895	
1.6	0.029	0.363	0.018	0.354	0.007	0.036	0.022	0.341	PANEL WT.
79.7	0.461	4.099	0.447	4.076	0.407	3,448	0.493	4.083	
1.6	-0.071	-0.177	-0.08	-0,174	0.071	1.489	-0.067	-0.192	PANEL WT.
105.7	0,808	4,829	0.818	4.78	0.764	4, 158	0.798	·4,758	
1.6	-0.123	-0.203	-0,132	-0.2	0.16	2,165	-0.131	-0.232	PANEL WT.
131.7	0.925	4.982	0.955	4.974	0.921	4.376	0.95		
1.6	0.118	2.647	0.082		0.121	2.501	0.114		PANEL WT.
157.8	1.055	5,233	1.116	****************	1.057	4.546	1.105		*******************
1.6	0.22	3.192	0.169	2,965	0.199	2.991	0.171	2.779	PANEL WT.
183.8	1.234	5.413	1.334	5.464	1.245	4,832	1.313		
1.6	0.477	4.342	0.436	4.185	0.337	3,416	0.418	4,038	PANEL WT.
209.8	1.423	5,675	1.548	5.753	1,464	5.09	1.526	*****	v#9%F:-
1.6	0.667	4.769	0.61	4.638	0.544	3.883	0.598	4.523	PANEL WT.
235,8	1.629	5,925	1.775	6.021	1.807	5.785	1.782	6.034	************************************
1.6	0.874	5,159	0.812	5.031	0,806	4,455	0.8		PANEL WT.
261.8	2,251	6.425	2.476	6.476	2.011	6.099	2.458		ULTIMATE
1.6	1.689	5.056	1.582	5,891	1.086	4.877	1,558	5.815	PANEL WT.

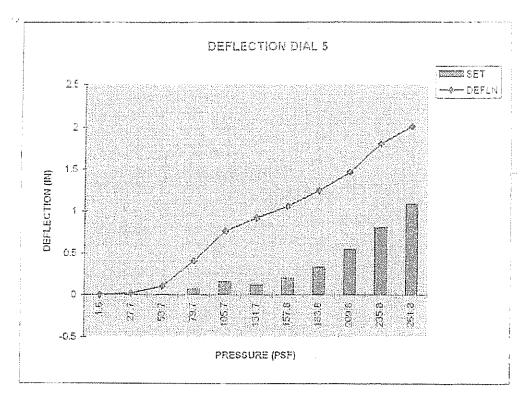
NOTE SEE SKETCH 4 FOR LOCATION OF SEAM DISENGAGEMENT.

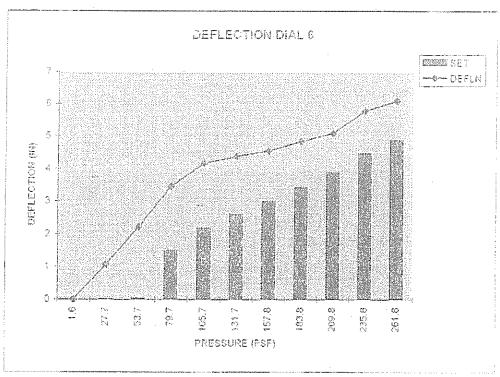


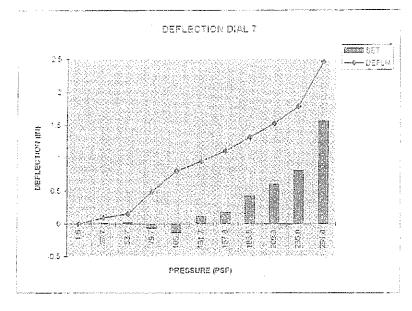


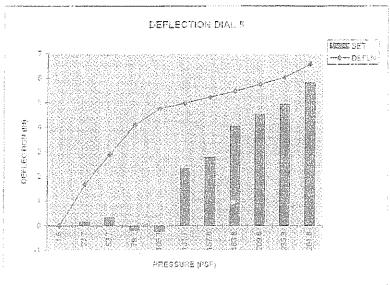


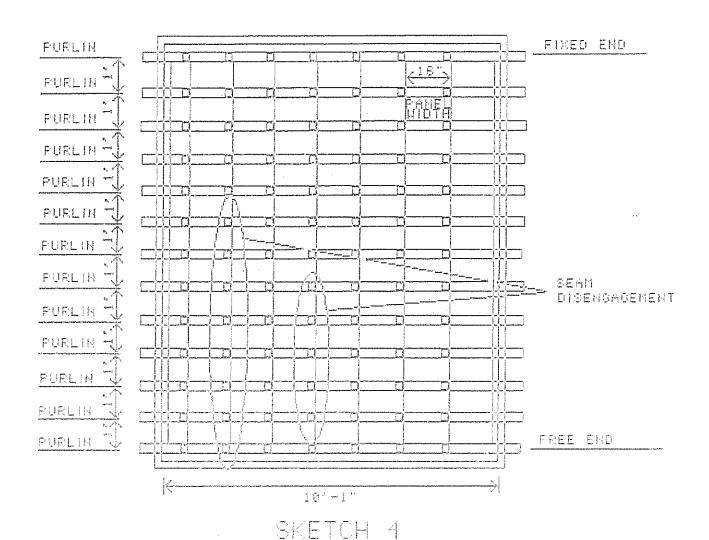






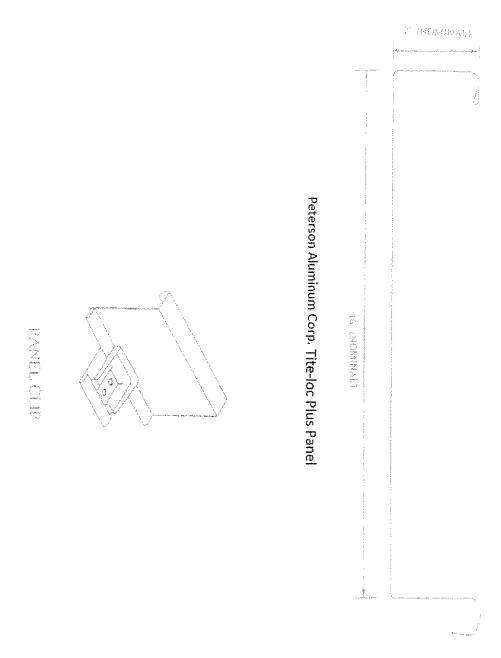


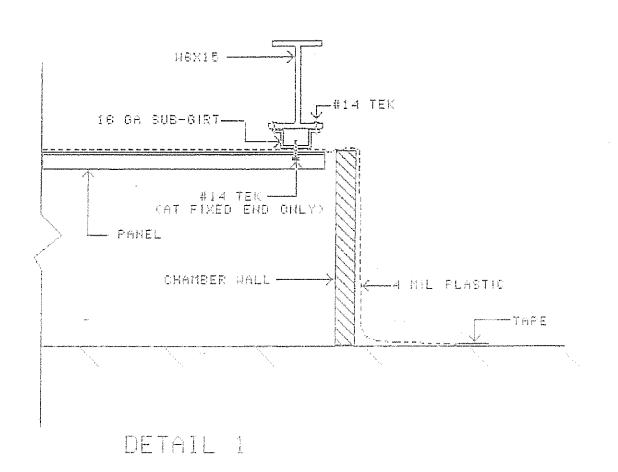


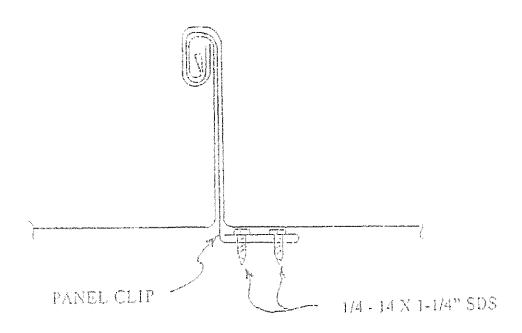


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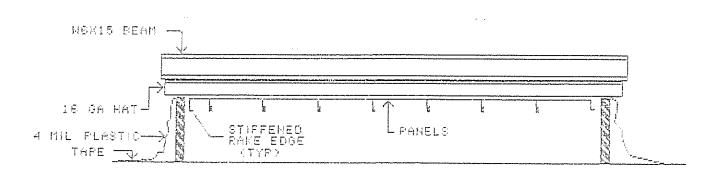
APPENDIX







DETAIL 2



SECTION A-A



THE SHOULDHOUGH SHEST

AN INDEPENDENT INSPECTION BUREAU AND TESTING LASONATORY

Keystone Cotumons ø 501 Braddock Ave. ø Turtle Greek, PA 15145-2084 PHONE: (412) 824-1900 - FAX: (412) 924-9785

File No. WP.9043 Report No. 055 Date: 12/12/97

REPORT OF TEASULE STRENGTH

Client. Farabangh Engineering & Testing

Date of Test Dec 11, 1997

Test Method: ASTM A-370

Fracture	8/0
Elongation (% in 2")	25.0
Tensile Strength (psi)	56,230
Field Point (psi)	49,590
Pensile Strength (Ibs.)	£98
Yedd Print (lbs)	SCO TO
Arca (sq.in)	0.0153
Neid Pensile Field Tensile Acts Prent Strength Point Strength Fracture (103) (103) (103) (103) (103) (103) (103)	0.0307 x 0.4999 22 ga.
The state of the s	MBCI 16" Superlok, 22 ga.

Tield Point determined by the Autographic / Halt-of-the-Load Method

Tost Equipment, ATS System 910 #A901779, Extensemeter #889016, Recorder #960709

fechnician D. Rupert

Respectfully submitted.

Todd A. Ault (M.E.T.) WEST PENN TESTING LABORATORIES, INC.